

Geometric design should not be considered complete nor should it be implemented until it has been determined that needed traffic devices will have the desired effect in controlling traffic.

Most of the intersection types illustrated and described in the following discussions are adaptable to either signing control, signal control, or a combination of both. At intersections that do not need signal control, the normal roadway widths of the approach highways are carried through the intersection with the possible addition of speed-change lanes, median lanes, auxiliary lanes, or pavement tapers. Where volumes are sufficient to indicate signal control, the number of lanes for through movements may also need to be increased. Where the volume approaches the uninterrupted flow capacity of the intersection leg, the number of lanes in each direction may have to be doubled at the intersection to accommodate the volume under stop-and-go control. Other geometric features that may be affected by signalization are length and width of storage areas, location and position of turning roadways, spacing of other subsidiary intersections, access connections, and the possible location and size of islands to accommodate signal posts or supports.

At high-volume intersections at grade, the design of the signals should be sophisticated enough to respond to the varying traffic demands, the objective being to keep the vehicles moving through the intersection. Factors affecting capacity and computation procedures for signalized intersections are covered in the HCM (6).

An intersection that needs traffic signal control is best designed by considering jointly the geometric design, capacity analysis, design hour volumes, and physical controls. Details on the design and location of most forms of traffic control signals, including the general warrants, are given in the MUTCD (9).

INTERSECTION SIGHT DISTANCE

General Considerations

Each intersection has the potential for several different types of vehicular conflicts. The possibility of these conflicts actually occurring can be greatly reduced through the provision of proper sight distances and appropriate traffic controls. The avoidance of conflicts and the efficiency of traffic operations still depend on the judgment, capabilities, and response of each individual driver.

Stopping sight distance is provided continuously along each highway or street so that drivers have a view of the roadway ahead that is sufficient to allow drivers to stop. The provision of stopping sight distance at all locations along each highway or street, including intersection approaches, is fundamental to intersection operation.

Vehicles are assigned the right-of-way at intersections by traffic-control devices or, where no traffic-control devices are present, by the rules of the road. A basic rule of the road, at an intersection where no traffic-control devices are present, requires the vehicle on the left to yield to the vehicle on the right if they arrive at approximately the same time. Sight distance is provided at

intersections to allow drivers to perceive the presence of potentially conflicting vehicles. This should occur in sufficient time for a motorist to stop or adjust their speed, as appropriate, to avoid colliding in the intersection. The methods for determining the sight distances needed by drivers approaching intersections are based on the same principles as stopping sight distance, but incorporate modified assumptions based on observed driver behavior at intersections.

The driver of a vehicle approaching an intersection should have an unobstructed view of the entire intersection, including any traffic-control devices, and sufficient lengths along the intersecting highway to permit the driver to anticipate and avoid potential collisions. The sight distance needed under various assumptions of physical conditions and driver behavior is directly related to vehicle speeds and to the resultant distances traversed during perception-reaction time and braking.

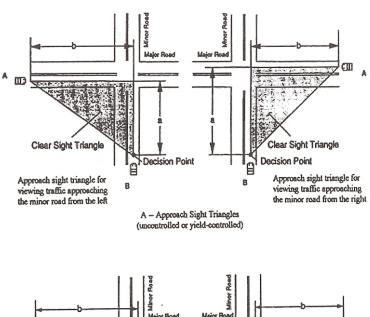
Sight distance is also provided at intersections to allow the drivers of stopped vehicles a sufficient view of the intersecting highway to decide when to enter the intersecting highway or to cross it. If the available sight distance for an entering or crossing vehicle is at least equal to the appropriate stopping sight distance for the major road, then drivers have sufficient sight distance to anticipate and avoid collisions. However, in some cases, this may require a major-road vehicle to stop or slow to accommodate the maneuver by a minor-road vehicle. To enhance traffic operations, intersection sight distances that exceed stopping sight distances are desirable along the major road.

Sight Triangles

Specified areas along intersection approach legs and across their included corners should be clear of obstructions that might block a driver's view of potentially conflicting vehicles. These specified areas are known as clear sight triangles. The dimensions of the legs of the sight triangles depend on the design speeds of the intersecting roadways and the type of traffic control used at the intersection. These dimensions are based on observed driver behavior and are documented by space-time profiles and speed choices of drivers on intersection approaches (10). Two types of clear sight triangles are considered in intersection design, approach sight triangles, and departure sight triangles.

Approach Sight Triangles

Each quadrant of an intersection should contain a triangular area free of obstructions that might block an approaching driver's view of potentially conflicting vehicles. The length of the legs of this triangular area, along both intersecting roadways, should be such that the drivers can see any potentially conflicting vehicles in sufficient time to slow or stop before colliding within the intersection. Exhibit 9-50A shows typical clear sight triangles to the left and to the right for a vehicle approaching an uncontrolled or yield-controlled intersection.



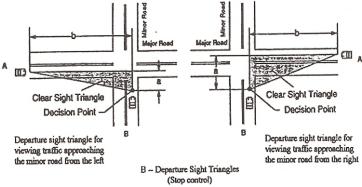


Exhibit 9-50. Intersection Sight Triangles

The vertex of the sight triangle on a minor-road approach (or an uncontrolled approach) represents the decision point for the minor-road driver (see Exhibit 9-50A). This decision point is the location at which the minor-road driver should begin to brake to a stop if another vehicle is present on an intersecting approach. The distance from the major road, along the minor road, is illustrated by the dimension "a" in Exhibit 9-50A.

The geometry of a clear sight triangle is such that when the driver of a vehicle without the right of way sees a vehicle that has the right of way on an intersecting approach, the driver of that potentially conflicting vehicle can also see the first vehicle. Dimension "b" illustrates the length of this leg of the sight triangle. Thus, the provision of a clear sight triangle for vehicles without the right-of-way also permits the drivers of vehicles with the right-of-way to slow, stop, or avoid other vehicles, should it become necessary.

Although desirable at higher volume intersections, approach sight triangles like those shown in Exhibit 9-50A are not needed for intersection approaches controlled by stop signs or traffic signals. In that case, the need for approaching vehicles to stop at the intersection is determined by

the traffic control devices and not by the presence or absence of vehicles on the intersecting approaches.

Departure Sight Triangles

A second type of clear sight triangle provides sight distance sufficient for a stopped driver on a minor-road approach to depart from the intersection and enter or cross the major road. Exhibit 9-50B shows typical departure sight triangles to the left and to the right of the location of a stopped vehicle on the minor road. Departure sight triangles should be provided in each quadrant of each intersection approach controlled by stop or yield signs. Departure sight triangles should also be provided for some signalized intersection approaches (see Case D in the section on "Intersection Control").

The recommended dimensions of the clear sight triangle for desirable traffic operations where stopped vehicles enter or cross a major road are based on assumptions derived from field observations of driver gap-acceptance behavior (10). The provision of clear sight triangles like those shown in Exhibit 9-50B also allows the drivers of vehicles on the major road to see any vehicles stopped on the minor-road approach and to be prepared to slow or stop, if necessary.

Identification of Sight Obstructions within Sight Triangles

The profiles of the intersecting roadways should be designed to provide the recommended sight distances for drivers on the intersection approaches. Within a sight triangle, any object at a height above the elevation of the adjacent roadways that would obstruct the driver's view should be removed or lowered, if practical. Such objects may include buildings, parked vehicles, highway structures, roadside hardware, hedges, trees, bushes, unmowed grass, tall crops, walls, fences, and the terrain itself. Particular attention should be given to the evaluation of clear sight triangles at interchange ramp/crossroad intersections where features such as bridge railings, piers, and abutments are potential sight obstructions.

The determination of whether an object constitutes a sight obstruction should consider both the horizontal and vertical alignment of both intersecting roadways, as well as the height and position of the object. In making this determination, it should be assumed that the driver's eye is 1 080 mm [3.5 ft] above the roadway surface and that the object to be seen is 1 080 mm [3.5 ft] above the surface of the intersecting road.

This object height is based on a vehicle height of 1 330 mm [4.35 ft], which represents the 15th percentile of vehicle heights in the current passenger car population less an allowance of 250 mm [10 in]. This allowance represents a near-maximum value for the portion of a passenger car height that needs to be visible for another driver to recognize it as the object. The use of an object height equal to the driver eye height makes intersection sight distances reciprocal (i.e., if one driver can see another vehicle, then the driver of that vehicle can also see the first vehicle).

Where the sight-distance value used in design is based on a single-unit or combination truck as the design vehicle, it is also appropriate to use the eye height of a truck driver in checking sight obstructions. The recommended value of a truck driver's eye height is 2 330 mm [7.6 ft] above the roadway surface.

Intersection Control

The recommended dimensions of the sight triangles vary with the type of traffic control used at an intersection because different types of control impose different legal constraints on drivers and, therefore, result in different driver behavior. Procedures to determine sight distances at intersections are presented below according to different types of traffic control, as follows:

Case A-Intersections with no control

Case B-Intersections with stop control on the minor road

Case B1-Left turn from the minor road

Case B2—Right turn from the minor road

Case B3—Crossing maneuver from the minor road

Case C—Intersections with yield control on the minor road

Case C1—Crossing maneuver from the minor road

Case C2-Left or right turn from the minor road

Case D-Intersections with traffic signal control

Case E-Intersections with all-way stop control

Case F-Left turns from the major road

Case A-Intersections with No Control

For intersections not controlled by yield signs, stop signs, or traffic signals, the driver of a vehicle approaching an intersection should be able to see potentially conflicting vehicles in sufficient time to stop before reaching the intersection. The location of the decision point (driver's eye) of the sight triangles on each approach is determined from a model that is analogous to the stopping sight distance model, with slightly different assumptions.

While some perceptual tasks at intersections may need substantially less time, the detection and recognition of a vehicle that is a substantial distance away on an intersecting approach, and is near the limits of the driver's peripheral vision, may take up to 2.5 s. The distance to brake to a stop can be determined from the same braking coefficients used to determine stopping sight distance in Exhibit 3-1.

Field observations indicate that vehicles approaching uncontrolled intersections typically slow to approximately 50 percent of their midblock running speed. This occurs even when no potentially conflicting vehicles are present (10). This initial slowing typically occurs at deceleration rates up to 1.5 m/s² [5 ft/s²]. Deceleration at this gradual rate has been observed to begin even before a potentially conflicting vehicle comes into view. Braking at greater deceleration rates, which can approach those assumed in stopping sight distance, can begin up to 2.5 s after a vehicle on the intersecting approach comes into view. Thus, approaching vehicles

may be traveling at less than their midblock running speed during all or part of the perception-reaction time and can, therefore, where necessary, brake to a stop from a speed less than the midblock running speed.

Exhibit 9-51 shows the distance traveled by an approaching vehicle during perception-reaction and braking time as a function of the design speed of the roadway on which the intersection approach is located. These distances should be used as the legs of the sight triangles shown in Exhibit 9-50A. Referring to Exhibit 9-50A, highway A with an assumed design speed of 80 km/h [50 mph] and highway B with an assumed design speed of 50 km/h [30 mph] require a clear sight triangle with legs extending at least 75 m and 45 m [245 and 140 ft] along highways A and B, respectively. Exhibit 9-52 indicates the length of the legs of the sight triangle from Exhibit 9-51.

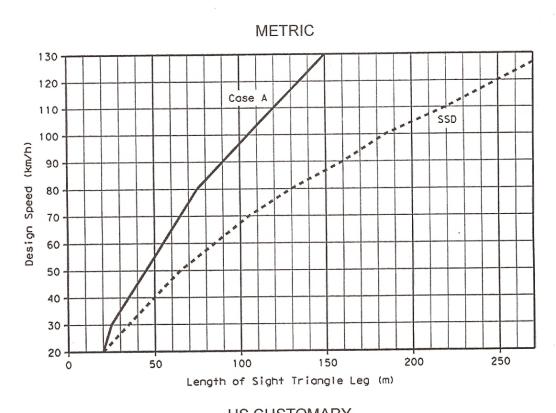
Me	etric	US Cus	tomary
Design speed	Length of leg	Design speed	Length of leg
(km/h)	(m)	(mph)	(ft)
20	20	15	70
30	25	20	90
40	35	25	115
50	45	30	140
60	55	35	165
70	65	40	195
80 90 100 110 120 130	75 90 105 120 135 150	45 50 55 60 65 70 75	220 245 285 325 365 405 445

Note: For approach grades greater than 3%, multiply the sight distance values in this exhibit by the appropriate adjustment factor from Exhibit 9-53.

Exhibit 9-51. Length of Sight Triangle Leg—Case A—No Traffic Control

This clear triangular area will permit the vehicles on either road to stop, if necessary, before reaching the intersection. If the design speed of any approach is not known, it can be estimated by using the 85th percentile of the midblock running speeds for that approach.

The distances shown in Exhibit 9-51 are generally less than the corresponding values of stopping sight distance for the same design speed. This relationship is illustrated in Exhibit 9-52. Where a clear sight triangle has legs that correspond to the stopping sight distances on their respective approaches, an even greater margin of efficient operation is provided. However, since field observations show that motorists slow down to some extent on approaches to uncontrolled intersections, the provision of a clear sight triangle with legs equal to the full stopping sight distance is not essential.



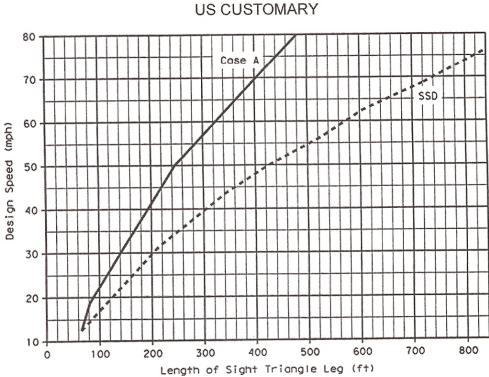


Exhibit 9-52. Length of Sight Triangle Leg—Case A—No Traffic Control

Where the grade along an intersection approach exceeds 3 percent, the leg of the clear sight triangle along that approach should be adjusted by multiplying the appropriate sight distance from Exhibit 9-51 by the appropriate adjustment factor from Exhibit 9-53.

If the sight distances given in Exhibit 9-51, as adjusted for grades, cannot be provided, consideration should be given to installing regulatory speed signing to reduce speeds or installing stop signs on one or more approaches.

No departure sight triangle like that shown in Exhibit 9-50B is needed at an uncontrolled intersection because such intersections typically have very low traffic volumes. If a motorist finds it necessary to stop at an uncontrolled intersection because of the presence of a conflicting vehicle on an intersecting approach, it is very unlikely another potentially conflicting vehicle will be encountered as the first vehicle departs the intersection.

Case B-Intersections with Stop Control on the Minor Road

Departure sight triangles for intersections with stop control on the minor road should be considered for three situations:

Case B1—Left turns from the minor road;

Case B2-Right turns from the minor road; and

Case B3—Crossing the major road from a minor-road approach.

Intersection sight distance criteria for stop-controlled intersections are longer than stopping sight distance to ensure that the intersection operates smoothly. Minor-road vehicle operators can wait until they can proceed safely without forcing a major-road vehicle to stop.

Case B1—Left Turn from the Minor Road

Departure sight triangles for traffic approaching from either the right or the left, like those shown in Exhibit 9-50B, should be provided for left turns from the minor road onto the major road for all stop-controlled approaches. The length of the leg of the departure sight triangle along the major road in both directions is the recommended intersection sight distance for Case B1.

The vertex (decision point) of the departure sight triangle on the minor road should be 4.4 m [14.5 ft] from the edge of the major-road traveled way. This represents the typical position of the minor-road driver's eye when a vehicle is stopped relatively close to the major road. Field observations of vehicle stopping positions found that, where necessary, drivers will stop with the front of their vehicle 2.0 m [6.5 ft] or less from the edge of the major-road traveled way. Measurements of passenger cars indicate that the distance from the front of the vehicle to the driver's eye for the current U.S. passenger car population is nearly always 2.4 m [8 ft] or less (10). Where practical, it is desirable to increase the distance from the edge of the major-road traveled way to the vertex of the clear sight triangle from 4.4 m to 5.4 m [14.5 to 18 ft]. This

Metric	US Customary
Approach Design speed (km/h)	Approach Design speed (mph)
20 30 40 50	grade (%) 15 20 25 30 35 40 45 50 55 60 65 70 75 80
	9
	-2
1.0 1.0 1.0 1.1 1.1 1.1 1.1 1.1 1.1 1.1	1.1 -4 1.0 1.0 1.0 1.1 1.1 1.1 1.1 1.1 1.1 1.1
1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	1.0 -3 to +3 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
44 10 10 10 10 0.9 0.9 0.9 0.9 0.9 0.9 0.9	0.9 +4 1.0 1.0 1.0 1.0 1.0 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9
+5 1.0 1.0 1.0 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9	0.9 +5 1.0 1.0 1.0 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0
1.0 1.0 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9	0.9 +6 1.0 1.0 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0.9 0

Note: Based on ratio of stopping sight distance on specified approach grade to stopping sight distance on level terrain.

Exhibit 9-53. Adjustment Factors for Sight Distance Based on Approach Grade

increase allows 3.0 m [10 ft] from the edge of the major-road traveled way to the front of the stopped vehicle, providing a larger sight triangle. The length of the sight triangle along the minor road (distance a in Exhibit 9-50B) is the sum of the distance from the major road plus 1/2 lane width for vehicles approaching from the left, or 1-1/2 lane width for vehicles approaching from the right.

Field observations of the gaps in major-road traffic actually accepted by drivers turning onto the major road have shown that the values in Exhibit 9-54 provide sufficient time for the minor-road vehicle to accelerate from a stop and complete a left turn without unduly interfering with major-road traffic operations. The time gap acceptance time does not vary with approach speed on the major road. Studies have indicated that a constant value of time gap, independent of approach speed, can be used as a basis for intersection sight distance determinations. Observations have also shown that major-road drivers will reduce their speed to some extent when minor-road vehicles turn onto the major road. Where the time gap acceptance values in Exhibit 9-54 are used to determine the length of the leg of the departure sight triangle, most major-road drivers should not need to reduce speed to less than 70 percent of their initial speed (10).

The intersection sight distance in both directions should be equal to the distance traveled at the design speed of the major road during a period of time equal to the time gap. In applying Exhibit 9-54, it can usually be assumed that the minor-road vehicle is a passenger car. However, where substantial volumes of heavy vehicles enter the major road, such as from a ramp terminal, the use of tabulated values for single-unit or combination trucks should be considered.

Exhibit 9-54 includes appropriate adjustments to the gap times for the number of lanes on the major road and for the approach grade of the minor road. The adjustment for the grade of the minor-road approach is needed only if the rear wheels of the design vehicle would be on an upgrade that exceeds 3 percent when the vehicle is at the stop line of the minor-road approach.

The intersection sight distance along the major road (dimension "b" in Exhibit 9-50B) is determined by:

	Metric	US Customary
	$ISD = 0.278 V_{major} t_g$	$ISD = 1.47 V_{major} t_g $ (9-1)
where:		where:
ISD $V_{\sf major}$	 intersection sight distance (length of the leg of sight triangle along the major road) (m) design speed of major 	ISD = intersection sight distance (length of the leg of sight triangle along the major road) (ft) $V_{ m major}$ = design speed of major
t_g	road (km/h) = time gap for minor road vehicle to enter the major road (s)	road (mph) t_g = time gap for minor road vehicle to enter the major road (s)

Design vehicle	Time gap (t_g) (seconds) at design speed of major road
Passenger car	7.5
Single-unit truck	9.5
Combination truck	11.5

Note: Time gaps are for a stopped vehicle to turn left onto a two-lane highway with no median and grades 3 percent or less. The table values require adjustment as follows:

For multilane highways:

For left turns onto two-way highways with more than two lanes, add 0.5 seconds for passenger cars or 0.7 seconds for trucks for each additional lane, from the left, in excess of one, to be crossed by the turning vehicle.

For minor road approach grades:

If the approach grade is an upgrade that exceeds 3 percent; add 0.2 seconds for each percent grade for left turns

Exhibit 9-54. Time Gap for Case B1—Left Turn from Stop

For example, a passenger car turning left onto a two-lane major road should be provided sight distance equivalent to a time gap of 7.5 s in major-road traffic. If the design speed of the major road is 100 km/h [60 mph], this corresponds to a sight distance of 0.278(100)(7.5) = 208.5 or 210 m [1.47(60)(7.5) = 661.5 or 665 ft], rounded for design.

A passenger car turning left onto a four-lane undivided roadway will need to cross two near lanes, rather than one. This increases the recommended gap in major-road traffic from 7.5 to 8.0 s. The corresponding value of sight distance for this example would be 223 m [706 ft]. If the minor-road approach to such an intersection is located on a 4 percent upgrade, then the time gap selected for intersection sight distance design for left turns should be increased from 8.0 to 8.8 s, equivalent to an increase of 0.2 s for each percent grade.

The design values for intersection sight distance for passenger cars are shown in Exhibit 9-55. Exhibit 9-56 includes design values, based on the time gaps for the design vehicles included in Exhibit 9-54.

No adjustment of the recommended sight distance values for the major-road grade is generally needed because both the major- and minor-road vehicle will be on the same grade when departing from the intersection. However, if the minor-road design vehicle is a heavy truck and the intersection is located near a sag vertical curve with grades over 3 percent, then an adjustment to extend the recommended sight distance based on the major-road grade should be considered.

	Ме	tric			US Cus	stomary	
		Intersectio				Intersection	n sight
	Stopping	distance	e for		Stopping	distance	e for
Design	sight	passenge	r cars	Design	sight	passenge	er cars
speed	distance	Calculated	Design	speed	distance	Calculated	Design
(km/h)	(m)	(m)	(m)	(mph)	(ft)	(ft)	(ft)
20	20	41.7	45	15	80	165.4	170
30	35	62.6	65	20	115	220.5	225
40	50	83.4	85	25	155	275.6	280
50	65	104.3	105	30	200	330.8	335
60	85	125.1	130	35	250	385.9	390
70	105	146.0	150	40	305	441.0	445
80	130	166.8	170	45	360	496.1	500
90	160	187.7	190	50	425	551.3	555
100	185	208.5	210	55	495	606.4	610
110	220	229.4	230	60	570	661.5	665
120	250	250.2	255	65	645	716.6	720
130	285	271.1	275	70	730	771.8	775
				75	820	826.9	830
				80	910	882.0	885

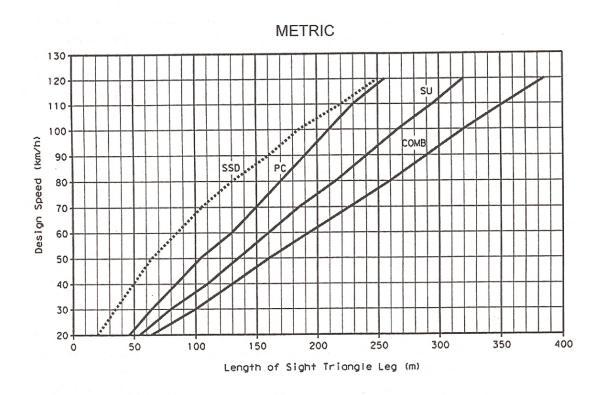
Note: Intersection sight distance shown is for a stopped passenger car to turn left onto a two-lane highway with no median and grades 3 percent or less. For other conditions, the time gap must be adjusted and required sight distance recalculated.

Exhibit 9-55. Design Intersection Sight Distance—Case B1—Left Turn from Stop

Sight distance design for left turns at divided-highway intersections should consider multiple design vehicles and median width. If the design vehicle used to determine sight distance for a divided-highway intersection is larger than a passenger car, then sight distance for left turns will need to be checked for that selected design vehicle and for smaller design vehicles as well. If the divided-highway median is wide enough to store the design vehicle with a clearance to the through lanes of approximately 1 m [3 ft] at both ends of the vehicle, no separate analysis for the departure sight triangle for left turns is needed on the minor-road approach for the near roadway to the left. In most cases, the departure sight triangle for right turns (Case B2) will provide sufficient sight distance for a passenger car to cross the near roadway to reach the median. Possible exceptions are addressed in the discussion of Case B3.

If the design vehicle can be stored in the median with adequate clearance to the through lanes, a departure sight triangle to the right for left turns should be provided for that design vehicle turning left from the median roadway. Where the median is not wide enough to store the design vehicle, a departure sight triangle should be provided for that design vehicle to turn left from the minor-road approach.

The median width should be considered in determining the number of lanes to be crossed. The median width should be converted to equivalent lanes. For example, a 7.2-m [24-ft] median should be considered as two additional lanes to be crossed in applying the multilane highway adjustment for time gaps in Exhibit 9-54. Furthermore, a departure sight triangle for left turns



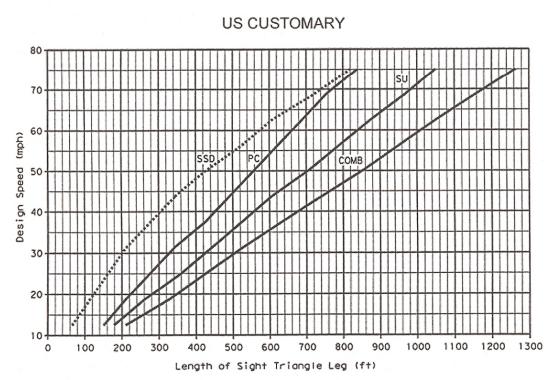


Exhibit 9-56. Intersection Sight Distance—Case B1—Left Turn from Stop

from the median roadway should be provided for the largest design vehicle that can be stored on the median roadway with adequate clearance to the through lanes. If a divided highway intersection has a 12-m [40-ft] median width and the design vehicle for sight distance is a 22-m [74-ft] combination truck, departure sight triangles should be provided for the combination truck turning left from the minor-road approach and through the median. In addition, a departure sight triangle should also be provided to the right for a 9-m [30-ft] single unit truck turning left from a stopped position in the median.

If the sight distance along the major road shown in Exhibit 9-55, including any appropriate adjustments, cannot be provided, then consideration should be given to installing regulatory speed signing on the major-road approaches.

Case B2—Right Turn from the Minor Road

A departure sight triangle for traffic approaching from the left like that shown in Exhibit 9-50B should be provided for right turns from the minor road onto the major road. The intersection sight distance for right turns is determined in the same manner as for Case B1, except that the time gaps (t_g) in Exhibit 9-54 should be adjusted. Field observations indicate that, in making right turns, drivers generally accept gaps that are slightly shorter than those accepted in making left turns (10). The time gaps in Exhibit 9-54 can be decreased by 1.0 s for right-turn maneuvers without undue interference with major-road traffic. These adjusted time gaps for the right turn from the minor road are shown in Exhibit 9-57. Design values based on these adjusted time gaps are shown in Exhibit 9-58 for passenger cars. Exhibit 9-59 includes the design values for the design vehicles for each of the time gaps in Exhibit 9-57. When the minimum recommended sight distance for a right-turn maneuver cannot be provided, even with the reduction of 1.0 s from the values in Exhibit 9-54, consideration should be given to installing regulatory speed signing or other traffic control devices on the major-road approaches.

Case B3—Crossing Maneuver from the Minor Road

In most cases, the departure sight triangles for left and right turns onto the major road, as described for Cases B1 and B2, will also provide more than adequate sight distance for minor-road vehicles to cross the major road. However, in the following situations, it is advisable to check the availability of sight distance for crossing maneuvers:

- where left and/or right turns are not permitted from a particular approach and the crossing maneuver is the only legal maneuver;
- where the crossing vehicle would cross the equivalent width of more than six lanes; or
- where substantial volumes of heavy vehicles cross the highway and steep grades that
 might slow the vehicle while its back portion is still in the intersection are present on
 the departure roadway on the far side of the intersection.

	Time gap (t_g) (seconds) at design
Design vehicle	speed of major road
Passenger car	6.5
Single-unit truck	8.5
Combination truck	10.5

Note: Time gaps are for a stopped vehicle to turn right onto or cross a two-lane highway with no median and grades 3 percent or less. The table values require adjustment as follows:

For multilane highways:

For crossing a major road with more than two lanes, add 0.5 seconds for passenger cars and 0.7 seconds for trucks for each additional lane to be crossed and for narrow medians that cannot store the design vehicle.

For minor road approach grades:

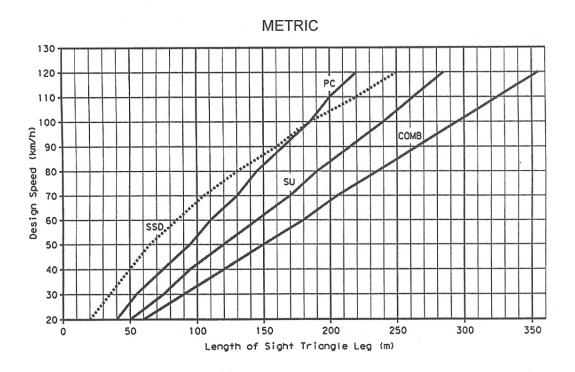
If the approach grade is an upgrade that exceeds 3 percent, add 0.1 seconds for each percent grade.

Exhibit 9-57. Time Gap for Case B2—Right Turn from Stop and Case B3—Crossing Maneuver

	M	etric			US Cu	stomary	
Design	Stopping sight	Intersection sight distance for passenger cars		Design	Stopping sight	Intersecti distand passeng	ce for er cars
speed	distance	Calculated	Design	speed	distance	Calculated	Design
(km/h)	(m)	(m)	(m)	(mph)	(ft)	(ft)	(ft)
20	20	36.1	40	15	80	143.3	145
30	35	54.2	55	20	115	191.1	195
40	50	72.3	75	25	155	238.9	240
50	65	90.4	95	30	200	286.7	290
60	85	108.4	110	35	250	334.4	335
70	105	126.5	130	40	305	382.2	385
80	130	144.6	145	45	360	430.0	430
90	160	162.6	165	50	425	477.8	480
100	185	180.7	185	55	495	525.5	530
110	220	198.8	200	60	570	573.3	575
120	250	216.8	220	65	645	621.1	625
130	285	234.9	235	70	730	668.9	670
130	200	20 1.0	200	75 80	820 910	716.6 764.4	720 765

Note: Intersection sight distance shown is for a stopped passenger car to turn right onto or cross a two-lane highway with no median and grades 3 percent or less. For other conditions, the time gap must be adjusted and required sight distance recalculated.

Exhibit 9-58. Design Intersection Sight Distance—Case B2—Right Turn from Stop and Case B3—Crossing Maneuver



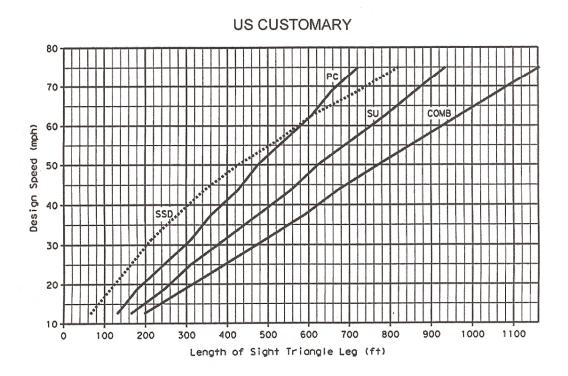


Exhibit 9-59. Intersection Sight Distance—Case B2—Right Turn from Stop and Case B3—Crossing Maneuver

The formula for intersection sight distance in Case B1 is used again for the crossing maneuver except that time gaps (t_g) are obtained from Exhibit 9-57. Exhibit 9-57 presents time gaps and appropriate adjustment factors to determine the intersection sight distance along the major road to accommodate crossing maneuvers. At divided highway intersections, depending on the relative magnitudes of the median width and the length of the design vehicle, intersection sight distance may need to be considered for crossing both roadways of the divided highway or for crossing the near lanes only and stopping in the median before proceeding. The application of adjustment factors for median width and grade is discussed under Case B1.

Exhibit 9-58 shows the design values for passenger cars for the crossing maneuver based on the unadjusted time gaps in Exhibit 9-57. Exhibit 9-59 includes the design values based on the time gaps for the design vehicles in Exhibit 9-57.

Case C-Intersections with Yield Control on the Minor Road

Drivers approaching yield signs are permitted to enter or cross the major road without stopping, if there are no potentially conflicting vehicles on the major road. The sight distances needed by drivers on yield-controlled approaches exceed those for stop-controlled approaches.

For four-leg intersections with yield control on the minor road, two separate pairs of approach sight triangles like those shown in Exhibit 9-50A should be provided. One set of approach sight triangles is needed to accommodate crossing the major road and a separate set of sight triangles is needed to accommodate left and right turns onto the major road. Both sets of sight triangles should be checked for potential sight obstructions.

For three-leg intersections with yield control on the minor road, only the approach sight triangles to accommodate left- and right-turn maneuvers need be considered, because the crossing maneuver does not exist.

Case C1—Crossing Maneuver from the Minor Road

The length of the leg of the approach sight triangle along the minor road to accommodate the crossing maneuver from a yield-controlled approach (distance *a* in Exhibit 9-50A) is given in Exhibit 9-60. The distances in Exhibit 9-60 are based on the same assumptions as those for Case A except that, based on field observations, minor-road vehicles that do not stop are assumed to decelerate to 60 percent of the minor-road design speed, rather than 50 percent.

Sufficient travel time for the major road vehicle should be provided to allow the minor-road vehicle: (1) to travel from the decision point to the intersection, while decelerating at the rate of 1.5 m/s^2 [5 ft/s²] to 60 percent of the minor-road design speed; and then (2) to cross and clear the intersection at that same speed. The intersection sight distance along the major road to accommodate the crossing maneuver (distance b in Exhibit 9-50A) should be computed with the following equations:

		Metric		U	S Customary
		$= t_a + \frac{w + L_a}{0.167V_{\text{minor}}}$ $= 0.278V_{major}t_g$			$t_a + \frac{w + L_a}{0.88V_{\text{minor}}} $ $.47V_{major}t_g $ (9-2)
where:			where:	-	
$egin{array}{c} t_g \ b \end{array}$	=	travel time to reach and clear the major road (s) length of leg of sight	b	= =	travel time to reach and clear the major road (s) length of leg of sight
t_a	=	triangle along the major road (m) travel time to reach the major road from the	t_a	=	triangle along the major road (ft) travel time to reach the major road from the
		decision point for a vehicle that does not stop (s) (use appropriate value for the minor-road design speed from Exhibit 9-60 adjusted for approach grade, where appropriate)	w		decision point for a vehicle that does not stop (s) (use appropriate value for the minor-road design speed from Exhibit 9-60 adjusted for approach grade, where appropriate) width of intersection to
W	=	width of intersection to be crossed (m)	L_a	=	be crossed (ft) length of design vehicle
L_a	=	length of design vehicle (m)	V_{minor}		(ft) design speed of minor
V_{minor}	=	design speed of minor road (km/h)	$V_{\sf major}$	=	road (mph) design speed of major
V_{major}	=	design speed of major road (km/h)	y major		road (mph)

The value of t_g should equal or exceed the appropriate travel time for crossing the major road from a stop-controlled approach, as shown in Exhibit 9-57. The design values for the time gap (t_g) shown in Exhibit 9-60 incorporate these crossing times for two-lane highways and are used to develop the length of the leg of the sight triangle along the major road in Exhibit 9-61. These basic unadjusted lengths are illustrated in Exhibit 9-62 for passenger cars and should be calculated separately for other design vehicle types.

The distances and times in Exhibit 9-60 should be adjusted for the grade of the minor-road approach using the factors in Exhibit 9-53. If the major road is a divided highway with a median wide enough to store the design vehicle for the crossing maneuver, then only crossing of the near lanes needs to be considered and a departure sight triangle for accelerating from a stopped position in the median should be provided based on Case B3. For median widths not wide enough to store the design vehicle, the crossing width should be adjusted as discussed in Case B1.

_	 															-			-	1
	(spuooes) (8		Design	value ^{3,4}	6.7	6.5	6.5	6.5	6.5	6.5	6.5	6.5	6.7	6.9	7.2	7.4	- 1	1.7	7.9	
nary	Travel time (t_g) (seconds)		Calculated	value	6.7	6.1	0.9	5.9	0.9	6.1	6.3	6.5	6.7	6.9	7.2	7 4	- 1	7.7	7.9	
US Customary	Minor-road approach	Travel time	$t_a^{-1,2}$	(seconds)	3.4	3.7	4.0	4.3	4.6	6.4	5.2	5.5	2.8	6.1	6.4	7	0.7	7.0	7.3	
	Minor-road	Length of	leg ¹	(#)	75	100	130	160	195	235	275	320	370	420	470	0 0	000	290	099	
		Design	peeds	(mph)	15	50	25	30	32	40	45	20	55	09) (C	9 6	2	75	80	
	(seconds)		Design	value ^{3,4}	7.1	6.5	6.5	6.5	6.5	, e	 	. c	7.1	7 4		- 0	α. Ω			
	Travel time $(t_arepsilon)$ (seconds)		Calculated	value	7.1	. 0	0 9	0.0		- o	o i r		7.5	7.7	†		0.8			
Metric	Minor-road approach	Travel time	1,2	(seconds)	3.0	i «	0.4	5.4	- α - ¬	i u	- ת	ب ن م) (1 0	0.	7.4			
	Minor-road	I enoth of		(E)	00	30	8 5	ት	S 4	8 8	000	2 5	10 L	2 1	200	180	202			
		Design	speed	(km/h)	200	0 6	3 5	4 n	200	9 6	2 6	8 8	200	2 7	0 0	02.1	130			

For minor-road approach grades that exceed 3 percent, multiply the distance or the time in this table by the appropriate adjustment factor from Exhibit 9-53.

Travel time applies to a vehicle that slows before crossing the intersection but does not stop. N

The value of t_g should equal or exceed the appropriate time gap for crossing the major road from a stop-controlled ന

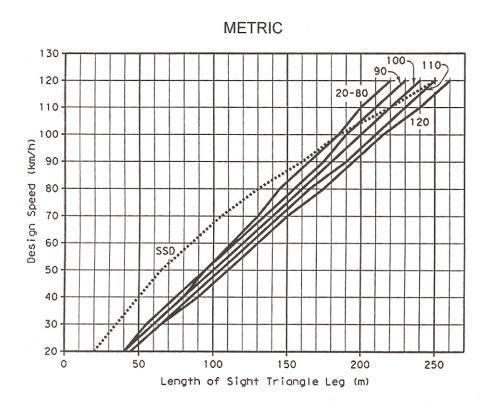
Values shown are for a passenger car crossing a two-lane highway with no median and grades 3 percent or less. 4

Exhibit 9-60. Case C1—Crossing Maneuvers from Yield-Controlled Approaches—Length of Minor Road Leg and Travel Times

Major road Stopping Stopping				Metric	<u>ပ</u> ု				1				US Customary	Istor	nary				
Stopping sight	Major						33	1950		Major	20	6				33.	3 G	\$P	
sight Minor-road design speed (km/h) sight speed (km/h) sight speed (km/h) sight speed (km/h) speed distance 20 30–80 90 100 110 120 130 (mp) (ft) Design values (ft) Design values (ft) Design values (ft) (mp) (ft) Design values (ft) Design values (ft) Design values (ft) (ft) Design values (ft) Design values (ft) (ft) Design values (ft) Design values (ft) Design values (ft) (ft) See 60 60 65 65 70 20 115 200 205 215 220 20 20 20 20 20 20 20 20 20 20 20 20	road									road	Stopping								
distance 20 30–80 90 100 110 120 130 (mph) (ft) Design values (ft) (mph) (ft) (ft) Design values (ft) (mph) (ft) (ft) Design values (ft) (mph) (ft) (ft) (ft) (ft) (ft) (ft) (ft) (ft	design			linor-rc	ad de	sign s	peed	(km/h)		design	sight		Minc	r-road	desi	gn spe	ed (m	ph)	
(m) Design values (m) (mph) (ft) Design values (ft) (mph) (ft) Design values (ft) (ft) (ft) Design values (ft) (ft) (ft) (ft) Design values (ft) (ft) (ft) (ft) (ft) (ft) (ft) (ft)	sbeed		20	30-80	90	100	110	120	130	sbeed	distance	12	20-50	55	09	65	2	75	8
20 40 40 46 45 45 45 45 46 570 66 66 66 66 66 70 20 115 200 195 200 205 206 <td>(km/h)</td> <td></td> <td></td> <td></td> <td>esign)</td> <td>value</td> <td></td> <td></td> <td></td> <td>(mph)</td> <td>(tt)</td> <td></td> <td></td> <td>De</td> <td>sign v</td> <td>_</td> <td>(#)</td> <td></td> <td></td>	(km/h)				esign)	value				(mph)	(tt)			De	sign v	_	(#)		
35 60 55 60 65 65 70 20 115 200 195 200 205 215 220 50 80 75 80 80 85 90 90 25 155 250 240 250 255 255 250 240 250 255 275 275 85 100 95 95 100 105 110 115 200 305 395 345 360 375 385 105 140 130 135 140 145 150 160 40 305 395 385 395 410 425 440 130 140 145 150 160 165 175 180 445 430 445 440 490 490 160 180 165 175 180 190 290 290 200 200 200 210	20	20	40	40	40	40	45	45	45	15	80	150	145	150		160	165	170	175
50 80 75 80 80 85 90 90 25 155 250 240 250 255 265 275 80 80 100 95 95 100 105 110 115 30 200 300 300 305 320 330 85 120 110 115 120 125 130 135 35 250 345 345 360 375 385 140 145 150 160 145 151 160 140 151 160 140 160 140 151 160 140 140 140 140 140 140 140 140 140 14	30	32	9	22	90	90	65	92	20	20	115	200				215	220	230	235
65 100 95 95 100 105 110 115 30 200 300 290 300 305 320 330 330 105 110 115 120 125 130 135 250 345 335 345 360 375 385 120 110 115 120 125 130 135 250 345 335 345 360 375 385 130 140 145 150 160 145 150 160 145 150 160 145 150 160 145 150 160 145 150 160 145 150 160 195 205 200 210 210 215 225 250 260 270 280 290 70 730 690 670 690 715 745 765 285 260 235 250 260 270 280 290 70 730 690 670 691 750 750 875 875 875 875 875 875 875 875 875 875	40	20	80	75	8	80	82	90	06	25	155	250				265	275	285	295
85 120 110 115 120 125 130 135 35 250 345 335 345 360 375 385 105 140 130 135 140 145 150 160 40 305 395 385 395 410 425 440 130 145 150 160 405 175 180 190 195 205 50 425 495 480 495 510 530 545 185 200 185 190 200 210 215 225 55 240 240 545 600 670 690 710 730 690 670 690 715 745 765 225 260 235 250 260 270 280 290 70 730 690 670 690 715 745 765 820 875 890 875 875 890 875 875 890 875 875 875 875 875 875 875 875 875 875	20	65	100	92	92	100	105	110	115	30	200	300				320	330	340	350
105 140 130 135 140 145 150 160 40 305 395 385 395 410 425 440 130 160 145 155 160 165 175 180 190 195 205 50 425 495 480 495 510 530 545 160 180 160 185 175 180 190 195 205 50 425 495 480 495 510 530 545 185 200 185 190 200 210 215 225 55 495 545 530 545 560 585 600 220 220 230 240 250 240 240 56 645 645 625 645 660 690 710 730 690 770 730 690 770 740 765 795 820 280 280 280 280 290 270 740 765 790 875 875 80 910 765 790 875 875 875	09	82	120	110	115	120	125	130	135	35	250	345		345		375	385	400	410
130 160 145 165 160 165 175 180 45 360 445 430 445 460 480 490	20	105	140	130	135	140	145		160	40	302	395				425	440	455	465
160 180 165 175 180 190 195 205 20 425 495 480 495 510 530 545 560 546 560 546 560 546 560 546 560 546 560 546 560 580 546 560 585 600 220 220 220 230 240 240 240 240 240 250 260 270 280 290 70 730 690 670 690 710 745 765 285 260 235 250 260 270 280 290 770 730 690 670 690 710 745 765 75 820 740 720 740 765 790 875 875	8	130	160	145	155	160	165		180	45	360	445				480	490	510	525
185 200 185 190 200 210 215 225 55 495 545 530 545 560 585 600 220 220 200 210 220 230 240 245 60 575 595 610 640 655 250 240 250 260 270 280 290 70 730 690 670 690 710 710 285 260 235 250 260 270 280 290 70 730 690 670 690 715 745 765 75 820 740 720 740 765 790 815 820	6	160	180	165	175	180	190		205	20	425	495				530	545	570	585
220 220 200 210 220 230 240 245 60 570 595 575 595 610 640 655 250 240 220 230 240 250 285 260 235 250 260 270 280 290 70 730 690 670 690 715 745 765 75 820 740 720 740 765 795 820 875 880 875 875 875 875 875 875 875 875 875 875	100	185	200	185	190	200	210		225	22	495	545				285	009	625	640
250 240 220 230 240 250 260 270	110	220		200	210	220	230		245	09	220	595				940	655	680	700
285 260 235 250 260 270 280 290 70 730 690 670 690 715 745 765 765 770 720 740 720 740 765 795 820 80 910 790 765 790 815 850 875	120	250		220	230	240	250		270	65	645	645				930	710	740	755
820 740 720 740 765 795 820 910 790 765 790 815 850 875	130	285		235	250	260	270		290	20	730	069			•	745	292	795	815
910 790 765 790 815 850 875										75	820	740	720		•	262	820	850	875
										80	910	790	765			350	875	910	930

Exhibit 9-60. The distances and times in Exhibit 9-60 need to be adjusted using the factors in Exhibit 9-53. Note: Values in the table are for passenger cars and are based on the unadjusted distances and times in

Exhibit 9-61. Length of Sight Triangle Leg along Major Road—Case C1—Crossing Maneuver at Yield Controlled Intersections



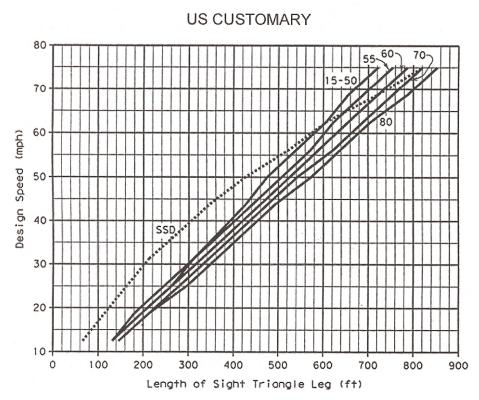


Exhibit 9-62. Length of Sight Triangle Leg along Major Road for Passenger Cars—Case C1—Crossing Maneuver

Case C2—Left- and Right-Turn Maneuvers

The length of the leg of the approach sight triangle along the minor road to accommodate left and right turns without stopping (distance a in Exhibit 9-50A) should be 25 m [82 ft]. This distance is based on the assumption that drivers making left and right turns without stopping will slow to a turning speed of 16 km/h [10 mph].

The leg of the approach sight triangle along the major road (distance b in Exhibit 9-50A) is similar to the major-road leg of the departure sight triangle for a stop-controlled intersections in Cases B1 and B2. However, the time gaps in Exhibit 9-54 should be increased by 0.5 s to the values shown in Exhibit 9-63. The appropriate lengths of the sight triangle leg are shown in Exhibit 9-64 for passenger cars and in Exhibit 9-65 for the general design vehicle categories. The minor-road vehicle needs 3.5 s to travel from the decision point to the intersection. This represents additional travel time that is needed at a yield-controlled intersection, but is not needed at a stop-controlled intersection (Case B). However, the acceleration time after entering the major road is 3.0 s less for a yield sign than for a stop sign because the turning vehicle accelerates from 16 km/h [10 mph] rather than from a stop condition. The net 0.5-s increase in travel time for a vehicle turning from a yield-controlled approach is the difference between the 3.5-s increase in travel time and the 3.0-s reduction in travel time.

Departure sight triangles like those provided for stop-controlled approaches (see Cases B1, B2, and B3) should also be provided for yield-controlled approaches to accommodate minor-road vehicles that stop at the yield sign to avoid conflicts with major-road vehicles. However, since approach sight triangles for turning maneuvers at yield-controlled approaches are larger than the departure sight triangles used at stop-controlled intersections, no specific check of departure sight triangles at yield-controlled intersection should be needed.

Yield-controlled approaches generally need greater sight distance than stop-controlled approaches, especially at four-leg yield-controlled intersections where the sight distance needs of the crossing maneuver should be considered. If sight distance sufficient for yield control is not available, use of a stop sign instead of a yield sign should be considered. In addition, at locations where the recommended sight distance cannot be provided, consideration should be given to installing regulatory speed signing or other traffic control devices at the intersection on the major road to reduce the speeds of approaching vehicles.

Case D—Intersections with Traffic Signal Control

At signalized intersections, the first vehicle stopped on one approach should be visible to the driver of the first vehicle stopped on each of the other approaches. Left-turning vehicles should have sufficient sight distance to select gaps in oncoming traffic and complete left turns. Apart from these sight conditions, there are generally no other approach or departure sight triangles needed for signalized intersections. Signalization may be an appropriate crash countermeasure for higher volume intersections with restricted sight distance that have experienced a pattern of sight-distance related crashes.

Design vehicle	Time gap (t_g) seconds
Passenger car	8.0
Single-unit truck	10.0
Combination truck	12.0

Note: Time gaps are for a vehicle to turn right or left onto a two-lane highway with no median. The table values require adjustments for multilane highways as follows:

For left turns onto two-way highways with more than two lanes, add 0.5 seconds for passenger cars or 0.7 seconds for trucks for each additional lane, from the left, in excess of one, to be crossed by the turning vehicle.

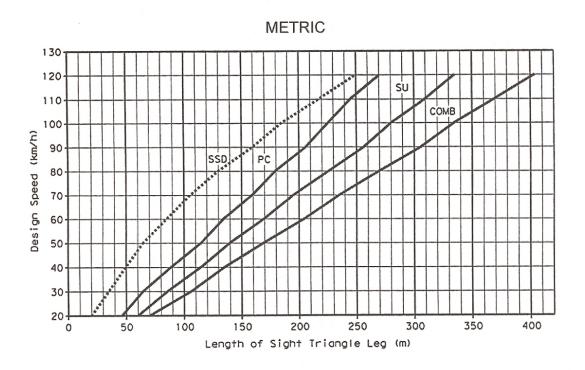
For right turns, no adjustment is necessary.

Exhibit 9-63. Time Gap for Case C2—Left or Right Turn

	Met	ric			US Cust	tomary	
		Length of	of leg			Length of	of leg
Design	Stopping	Passenge	er cars	Design	Stopping	Passenge	er cars
speed	sight	Calculated	Design	speed	sight	Calculated	Design
(km/h)	distance (m)	(m)	(m)	(mph)	distance (ft)	(ft)	(ft)
20	20	44.5	45	15	80	176.4	180
30	35	66.7	70	20	115	235.2	240
40	50	89.0	90	25	155	294.0	295
50	65	111.2	115	30	200	352.8	355
60	85	133.4	135	35	250	411.6	415
70	105	155.7	160	40	305	470.4	475
80	130	177.9	180	45	360	529.2	530
90	160	200.2	205	50	425	588.0	590
100	185	222.4	225	55	495	646.8	650
110	220	244.6	245	60	570	705.6	710
120	250	266.9	270	65	645	764.4	765
130	285	289.1	290	70	730	823.2	825
				75	820	882.0	885
	3.	10.	N 12 - 12 - 1	80	910	940.8	945

Note: Intersection sight distance shown is for a passenger car making a right or left turn without stopping onto a two-lane road.

Exhibit 9-64. Design Intersection Sight Distance—Case C2—Left or Right Turn at Yield-Controlled Intersections



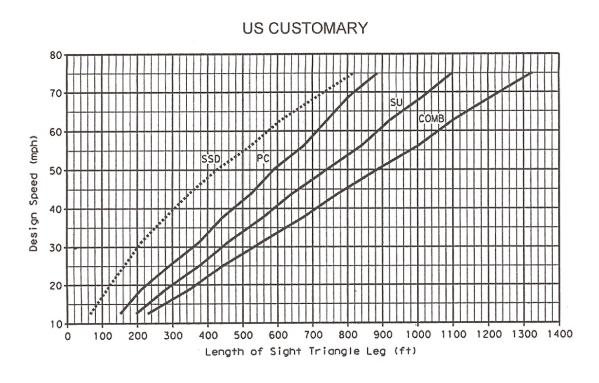


Exhibit 9-65. Intersection Sight Distance—Case C2—Yield-Controlled Left or Right Turn

However, if the traffic signal is to be placed on two-way flashing operation (i.e., flashing yellow on the major-road approaches and flashing red on the minor-road approaches) under off-peak or nighttime conditions, then the appropriate departure sight triangles for Case B, both to the left and to the right, should be provided for the minor-road approaches. In addition, if right turns on a red signal are to be permitted from any approach, then the appropriate departure sight triangle to the left for Case B2 should be provided to accommodate right turns from that approach.

Case E-Intersections with All-Way Stop Control

At intersections with all-way stop control, the first stopped vehicle on one approach should be visible to the drivers of the first stopped vehicles on each of the other approaches. There are no other sight distance criteria applicable to intersections with all-way stop control and, indeed, all-way stop control may be the best option at a limited number of intersections where sight distance for other control types cannot be attained.

Case F—Left Turns from the Major Road

All locations along a major highway from which vehicles are permitted to turn left across opposing traffic, including intersections and driveways, should have sufficient sight distance to accommodate the left-turn maneuver. Left-turning drivers need sufficient sight distance to decide when it is safe to turn left across the lane(s) used by opposing traffic. Sight distance design should be based on a left turn by a stopped vehicle, since a vehicle that turns left without stopping would need less sight distance. The sight distance along the major road to accommodate left turns is the distance traversed at the design speed of the major-road in the travel time for the design vehicle given in Exhibit 9-66.

Design vehicle	Time gap (t_g) (seconds) at design speed of major road
Passenger car	5.5
Single-unit truck	6.5
Combination truck	7.5

Adjustment for multilane highways:

For left-turning vehicles that cross more than one opposing lane, add 0.5 seconds for passenger cars and 0.7 seconds for trucks for each additional lane to be crossed.

Exhibit 9-66. Time Gap for Case F—Left Turns from the Major Road

The table also contains appropriate adjustment factors for the number of major-road lanes to be crossed by the turning vehicle. The unadjusted time gap in Exhibit 9-66 for passenger cars was used to develop the sight distances in Exhibit 9-67 and illustrated in Exhibit 9-68.

	Me	tric		US Customary				
		Intersectio distan				Intersectio distan	- 1	
Design	Stopping	Passenge	er cars	Design	Stopping	Passenger cars		
speed (km/h)	sight distance (m)	Calculated (m)	Design (m)	speed (mph)	sight distance (ft)	Calculated (ft)	Design (ft)	
20	20	30.6	35	15	80	121.3	125	
30	35	45.9	50	20	115	161.7	165	
40	50	61.2	65	25	155	202.1	205	
50	65	76.5	80	30	200	242.6	245	
60	85	91.7	95	35	250	283.0	285	
70	105	107.0	110	40	305	323.4	325	
80	130	122.3	125	45	360	363.8	365	
90	160	137.6	140	50	425	404.3	405	
100	185	152.9	155	55	495	444.7	445	
110	220	168.2	170	60	570	485.1	490	
120	250	183.5	185	65	645	525.5	530	
130	285	198.8	200	70	730	566.0	570	
				75	820	606.4	610	
				80	910	646.8	650	

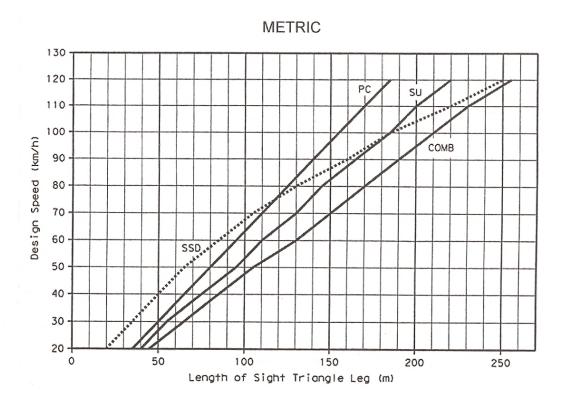
Note: Intersection sight distance shown is for a passenger car making a left turn from an undivided highway. For other conditions and design vehicles, the time gap should be adjusted and the sight distance recalculated.

Exhibit 9-67. Intersection Sight Distance—Case F—Left Turn from Major Road

If stopping sight distance has been provided continuously along the major road and if sight distance for Case B (stop control) or Case C (yield control) has been provided for each minor-road approach, sight distance will generally be adequate for left turns from the major road. Therefore, no separate check of sight distance for Case F may be needed.

However, at three-leg intersections or driveways located on or near a horizontal curve or crest vertical curve on the major road, the availability of adequate sight distance for left turns from the major road should be checked. In addition, the availability of sight distance for left turns from divided highways should be checked because of the possibility of sight obstructions in the median.

At four-leg intersections on divided highways, opposing vehicles turning left can block a driver's view of oncoming traffic. Exhibit 9-98, presented later in this chapter, illustrates intersection designs that can be used to offset the opposing left-turn lanes and provide left-turning drivers with a better view of oncoming traffic.



US CUSTOMARY SU сомв Design Speed (mph) SSD

Exhibit 9-68. Intersection Sight Distance—Case F—Left Turn from Major Road

Length of Sight Triangle Leg (ft)

Effect of Skew

When two highways intersect at an angle less than 60 degrees, and when realignment to increase the angle of intersection is not justified, some of the factors for determination of intersection sight distance may need adjustment.

Each of the clear sight triangles described above are applicable to oblique-angle intersections. As shown in Exhibit 9-69, the legs of the sight triangle will lie along the intersection approaches and each sight triangle will be larger or smaller than the corresponding sight triangle would be at a right-angle intersection. The area within each sight triangle should be clear of potential sight obstructions as described previously.

At an oblique-angle intersection, the length of the travel paths for some turning and crossing maneuvers will be increased. The actual path length for a turning or crossing maneuver can be computed by dividing the total widths of the lanes (plus the median width, where appropriate) to be crossed by the sine of the intersection angle. If the actual path length exceeds the total widths of the lanes to be crossed by 3.6 m [12 ft] or more, then an appropriate number of additional lanes should be considered in applying the adjustment for the number of lanes to be crossed shown in Exhibit 9-54 for Case B1 and in Exhibit 9-57 for Cases B2 and B3. For Case C1, the *w* term in the equation for the major-road leg of the sight triangle to accommodate the crossing maneuver should also be divided by the sine of the intersection angle to obtain the actual path length. In the obtuse-angle quadrant of an oblique-angle intersection, the angle between the approach leg and the sight line is often so small that drivers can look across the full sight triangle with only a small head movement. However, in the acute-angle quadrant, drivers are often required to turn their heads considerably to see across the entire clear sight triangle. For this reason, it is recommended that the sight distance criteria for Case A not be applied to oblique-angle intersections and that sight distances at least equal to those for Case B should be provided, whenever practical.

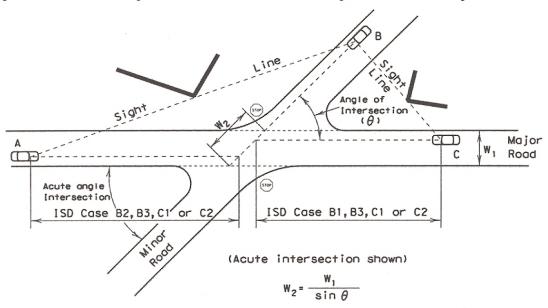


Exhibit 9-69. Sight Triangles at Skewed Intersections

STOPPING SIGHT DISTANCE AT INTERSECTIONS FOR TURNING ROADWAYS

General Considerations

The values for stopping sight distance as computed in Chapter 3 for open highway conditions are applicable to turning roadway intersections of the same design speed. The values from Chapter 3, together with the value for a design speed of 15 km/h [10 mph]), are shown in Exhibit 9-70. These distances have been rounded upward to provide an increased factor of safety.

Metric								US Customary
(km/h)								Design speed 10 15 20 25 30 35 40 45 (mph)
Stopping sight distance (m)	15	20	35	50	65	85	105	Stopping sight 50 80 115 155 200 250 305 360 distance (ft)

Exhibit 9-70. Stopping Sight Distance for Turning Roadways

These sight distances should be available at all points along a turning roadway; wherever practical, longer sight distances should be provided. They apply as controls in design of both vertical and horizontal alignment.

Vertical Control

The length of vertical curve is predicated, as it is for open highway conditions, on sight distance measured from the height of eye of 1 080 mm [3.5 ft] to the height of object of 600 mm [2 ft]. Formulas shown in the section on "Crest Vertical Curves" in Chapter 3 apply directly. Exhibits 3-71 and 3-72 show the relation between design speed, algebraic difference in gradient, and length of crest vertical curve to provide stopping distance. The factor K is constant for each design speed and the length of vertical curve is found by multiplying A, the algebraic differences in percent of grades, by K.

For design speeds of less than 60 km/h [40 mph], sag vertical curves, as governed by headlight sight distances, theoretically should be longer than crest vertical curves. Lengths of sag vertical curves are found by substituting the stopping sight distances from Exhibit 9-70 in the formulas in the section on "Sag Vertical Curves" in Chapter 3. Because the design speed of most turning roadways is governed by the horizontal curvature and the curvature is relatively sharp, a headlight beam parallel to the longitudinal axis of the vehicle ceases to be a control. Where practical, longer lengths for both crest and sag vertical curves should be used.

Horizontal Control

The sight distance control as applied to horizontal alignment has an equal, if not greater, effect on design of turning roadways than the vertical control. The sight line along the centerline 678

of the inside lane around the curve, clear of obstructions, should be such that the sight distance measured on an arc along the vehicle path equals or exceeds the stopping sight distance given in Exhibit 9-70. A likely obstruction may be a bridge abutment or line of columns, wall, cut sideslope, or a side or corner of a building.

The lateral clearance, centerline of inside lane to sight obstruction, for various radii and design speeds, is shown in Exhibit 3-53. The lateral clearances shown in this exhibit apply to the conditions where the horizontal curve is longer than the stopping sight distance. Where the curve length is shorter than the sight distance control, the lateral clearance of Exhibit 3-53 results in greater sight distance. In this case the lateral clearance is best determined by scaling on a plan layout of the turning roadway in a manner indicated by the sketch in Exhibit 3-8 or 3-54. The lateral clearance, so determined, should be tested at several points.

DESIGN TO DISCOURAGE WRONG-WAY ENTRY

An inherent problem of interchanges is the possibility of a driver entering one of the exit terminals from the crossroad and proceeding along the major highway in the wrong direction in spite of signing. This wrong-way entrance maneuver is becoming more of a problem with the increased number of interchanges. However, attention to several details of design at the intersection can discourage this maneuver.

As shown in Exhibits 9-71 and 9-72, a sharp or angular intersection is provided at the junction of the left edge of the ramp entering the crossroad and the right edge of the traveled way. The control radius should be tangent to the crossroad centerline, not the edge. This type of design discourages the improper right turn onto the one-way ramp.

As shown in the same figures, islands can be used in the terminal areas where ramps intersect the crossroads. The islands provide a means of channelizing the traffic into proper paths and can be effectively used for sign placement. Design of the islands should take into consideration initial or future signal installations at the ramp terminals.

Provision of a median as a deterrent to wrong-way movement, as illustrated in Exhibit 9-72, is a very effective treatment. The median makes the left-turn movement onto the exit ramp terminal very difficult, and a short-radius curve or angular break is provided at the intersection of the left edge of the exit ramp and the crossroad to discourage wrong-way right turns from the crossroads.

Additional design techniques to reduce wrong-way movements are (1) providing for all movements to and from the freeway to reduce intentional wrong-way entry, (2) using conventional, easily recognized interchange patterns to reduce driver confusion and hence wrong-